

The Influence of Position and Number of Longitudinal Connection of Sengon Glulam Beams Towards Strength and Stiffness

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Abstract - The demand of wood as construction material always increases. However, sawn-wood with large size is more difficult to find in the market due to decreasing in stock dimension. In addition, it makes price more expensive. Indonesia has many trees from fast-growing species: however, they have low wood quality, and still limited in usage. To obtain a better performance of fast-growing species as construction material, it needs to be combined to produce glulam. This research observed the influence of position and longitudinal connections of wood glulam beam on strength and stiffness with damage species of sengonglulam beams. Preliminary testing was done to obtain physical and mechanical properties of clear specimen of sengon wood, testing method followed ISO-1995 standard. Fifteen glulam beam specimens which had 70 mm wide, 200 mm depth, 3000 mm length were constructed: They represented variations of position and connection work of 0 %, 25 %, 50 %, 75 % and 100 %. Each layer of lumber glued with thermosetting phenol formaldehyde (PA-302) adhesive at pressure 1 up to 1,1MPa for 10 hour pressing time. The static lateral loading steps were done continuously until the beam was damaged. The result indicated that sengon was V class of strength. Glulam testing showed that in terms of strength and stiffness, the higher the number of connections, the lower the value. The strength reduction percentages of 0%, 25%, 50%, 75% and 100% produced 0%, 13,08%, 28,11%, 29,42%, 70,72 %. Respectively and the degradation of glulam stiffness were 100%, 99,92%, 87,86%, 83,06%, 67,08%. The failure of glulam beam with 0% had a shear followed by flexure damages of 25%, 50%, 75% and 100%. A flexure damage was followed by shear damage.

Keywords: *Paraserianthesfalcataria, Connection, Glulam Beam, Strength, Stiffness.*

1. Introduction

Wood is one of the renewable natural resources. It has been used as a construction material for a very long time, before the technology of concrete and steel was developed. Besides meeting architectural demands, wood has several advantages including: great strength, lightweight, earthquake resistant, easy to implement, and relative cheap in some areas. Structural wood is widely applied in the construction of roofs, building frames, bridge girders, train bearings and so on. The need of processed wood as a construction material always increases. According to Susetyowati and Subianto (1998), each year for about not less than 3 million cubic meters of sawn timber is needed for the construction of housing, buildings and others in Indonesia. However, to obtain good quality sawn timber, the relatively large size wood is increasingly difficult to find in the market due to the depletion of natural forest production.

According to Syafi'i (1998), in the future, it is estimated that the potential of wood and natural forest area in Indonesia is decreasing, so the supply of wood raw material is from the production of industrial timber plantation (HTI). The efforts to improve the efficiency of wood's use can be done by using fast-growing wood species that generally have small diameter and low quality. Some developed countries continue to develop glulam beam product with low quality wood type. Glulam Beam is a combination of some woods into a whole. It also has more advantages than solid sawmill timber, great

strength, smaller deformation, and larger and longer sections. The utilization of glulam beams with low quality wood will save high quality wood and construction cost. Some studies that have been conducted include: Kasmudjo (1995) which examined the strength of sengon wood adhesive for laminated board, Sutigno et al. (1991) examined the effect of the connection on the mechanical properties will increase when the number of layer increases in sengon wood, Fakri (2000) examined the effect of the number of wood that fills the kruing-sengon glulam beam against strength and stiffness with Urea Formaldehyde resin.

2. How to Research

This research used 160 sheet of sengon wood from Ambarawa with the size of 3 cm x 8 cm x 3.4m and used Phenol Formaldehyde adhesive from PT. Pamolite Adhesive Industry, Probolinggo, East Java. The drying of sengon wood was done naturally in the wood processing laboratory of Faculty of Forestry UGM. The woods were arranged so that the air flowed in the wood arrangement until it reached 12 percent of moisture content measured by a Moisture Content tool. After the moisture content was reached, the glulam beam was made. The test of physical and mechanical properties was done in accordance with ISO 1995 standards and 36 samples were stated defect-free wood. It included the test of moisture content, density, parallel and perpendicular fibers pressure, bending (MOR), elastic modulus, parallel fibertensile, laminated shear beam with adhesive spreads of 40/MDGL, 60/MDGL, 80/MDGL, and the test of connection tensile which were done three times for each test.

Before glulam beam was made, laminate shear beam test was done with adhesive variations of 40/MDGL, 60/MDGL, 80/MDGL with 3 samples and its correction in each. From the test, it was found that the optimum adhesive spread was 60/MDGL. Then, 15 glulam beams were made. Dry wood boards with for about 12 percent of moisture content which had been shredded were glued and forged in 1 to 1.1 MPa for 10 hours. The making of wood connection was done before the glulam beam was pressed. Position variation and number of connections on glulam beam were 0%, 25%, 50%, 75%, 100%.

The process of physical and mechanical properties test, density and moisture content test were implemented in physics and mechanics laboratory of Faculty of Forestry Universitas GadjahMada. The test of the mechanical properties of wood was done in the laboratory of mechanical materials of Engineering Sciences UGM by using moisture meter, oven, scales, caliper and Unistated Testing System (UTS).

Glulam beam testing was done in mechanical laboratory of PAU material, UGM, by using frame tool, dial gauge to measure deflection, transducer to know the loading stages, load cell with 10 ton capacity, 15 ton capacity of Jack Hydraulic to give load on the specimen. The test was done after setting the tools and the test object. 50 kg load was given gradually. The deflection read on the dial gauge was noted. Loading was done until collapse occurred.



Picture 1: The Image of Glulam Beam Test.

3. Research Result and Discussion

The test results of physical and mechanical properties can be seen in table 3. Flexural strength was less than 36 MPa and compressive strength was less than 21.5 MPa. Based on its strength, sengon wood belongs to class V. The shear strength was 4.41 MPa in average to resist the horizontal shear force of external load. Short span style laminate wood has the biggest shear force on the axis of the cross section so that the dominant fails to shear.

Table 1. Test Results of Physical and Mechanical Properties

No	Density (t/m ³)	Moisture Content (%)	Wood strength						Strength Class
			Flexure (Mpa)	Pressure (Mpa)	Pressure (Mpa)	tensile (Mpa)	Connection tensile (Mpa)	Shear (Mpa)	
1.	0.263	11.95	34.21	16.78	5.43	66.78	11.87	3.73	V
2.	0.289	14.22	32.41	18.58	3.79	85.49	6.11	4.64	V
3.	0.262	14.43	30.28	16.19	4.28	83.44	10.21	4.85	V

It can be seen from the table above that tensile strength of the connection was 9.39 Mpa lower than the tensile strength without connection. It will weaken the glulam beam if the connection is in the tensile region. The glulam beam shear strength with the adhesive of 40/MDGL, 60/MDGL, 80/MDGL was obtained average shear strength of 0.901 MPa, 2.512 MPa, 1,983 MPa and retrieved 0.755 MPa, 2,247 MPa, 1,971 MPa in the following tests. It was found that the optimal glulam beam adhesive was 60/MDGL.

4. The Strength of Glulam Beam

The test results of all variations of position and number of connections from 0%, 25%, 50%, 75% and 100% obtained the average load of the proportional limit, the initial collapse load, the peak load and the decreasing collapsed load so that the beam strength obtained was decreased. The position and number of connections in longitudinal direction were decreased by 89.54%, 81.17%, 84.72%, 83.62%, and 78.45%. The average decrease of load can be seen in table. 2. It was found that the more the position and the number of connection, the smaller the strength of glulam beam.

Table 2. Recapitulation of Glulam Beam Test Results Load

No.	Beam Code	Average load				The average of proportional limit Toward Peak load (%)
		Proportional Limit	initial damage	Peak	collapse	
		(N)	(N)	(N)	(N)	
1	BLS 00	21000	21500	25500	2566,67	89,54
2	BLS 25	16333,34	16833,34	22166,67	22166,67	81,17
3	BLS 50	15500	16333,34	18333,34	18500	84,72
4	BLS -75	14833,34	15666,67	18000	18166,67	83,67
5	BLS- 100	5866,67	6400	7466,67	7566,67	78,45

The percentage decreases in average strength of glulam beam in various positions and the number of connections were 0%, 25%, 50%, 75%, and 100%. It was obtained average power loss of 0%, 13.08%, 28.11%, 29.42%, and 70.72%. It can be seen in table 3 below. It was found that the more variation in position and number of connections, the smaller the power. For connection of 25%, the power loss was very small for about 13.08%. It meant that connection of 25% could still be used on the glulam beam.

Table 3. Reduction of Glulam beam strength

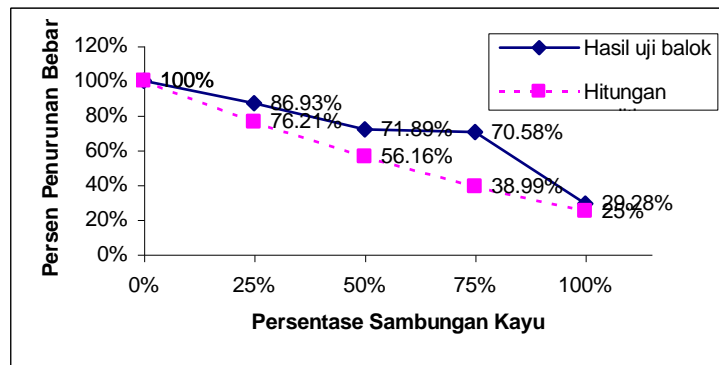
No.	Beam Code	Maximum load		Percentage toward BLS 00 (%)	Power Loss (%)
		Average	Average		
		(Kg)	(N)		
1	BLS 00	2550,00	25500,00	100	0.00
2	BLS 25	2216,667	22166,67	86.92	13.08
3	BLS 50	1833,334	18333,34	71.89	28.11
4	BLS 75	1816,667	18166,67	70.58	29.42
5	BLS 100	756,667	7566,67	29.28	70.72

The percentage decreases of glulam beam load from test result compared to percentage decrease of load result of the theoretical calculation for various positions and number of longitudinal direction length were 0%, 25%, 50%, 75%, and 100%. On beam test result, it was obtained sequential load decreases equal to 100 %, 86.93%, 71.89%, 70.58%, and 29.28%. Theoretically, it was obtained sequential load decreases of 100%, 76.21%, 56.16%, 38.99%, and 25.05%. It was found that between glulam and theoretical beam test there was a difference of the load decrease percentages in sequence according to the position and the number of connections by 0%, 10.72%, 15.73%, 31.59%, and 4.23%. Based on this very small difference, it meant that the count results did not exceed the limits of glulam beam strength. It is shown Table 4 and Figure 2.

Table 4. The decrease of glulam and theoretical beam load

N0	Beam code	Peak load of the test Average	Test result decrease	Peak load of the theoretical Average	Theoretical result decrease
		(N)	(%)	(N)	(%)
1	BLS 00	25500.00	100%	15380.6699	100%
2	BLS 25	22166.67	86.93%	11720.8827	76.21%
3	BLS-50	18333.34	71.89%	8638.0294	56.16%

N0	Beam code	Peak load of the test Average (N)	Test result decrease (%)	Peak load of the theoretical Average (N)	Theoretical result decrease (%)
4	BLS 75	18000.00	70.58%	5997.2016	38.99%
5	BLS-100	7466.67	29,28%	3852.8517	25.05%

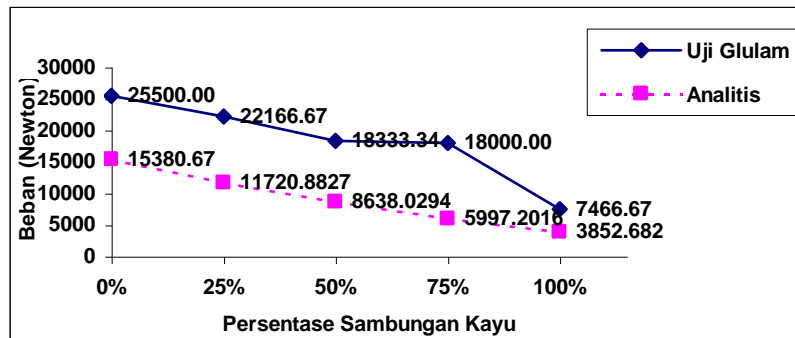


Picture 2: Percentage Of Glulam And Theoretical Load Decreases

To determine the strength of the beam theoretically, the capacity analysis was done and found that the average moment was decreased sequentially as 7690.335 Nm, 5860.441 Nm, 4324.162 Nm, 2981.44 Nm, and 1927.341 Nm. The averages of decrease in the analytical load were 15380.6 N, 11720.8 N, 8638.2 N, and 3852.6 N. The shear forces corresponding to the variation in positions and number of longitudinal directions are shown in Table 5 and from FIG. 3. It was obtained decrease averages of beam analytical of 0%, 25%, 50%, 75%, 100% by 60,31%, 52,87%, 47,12%, 33,32% and 51,59%.

Table 5. Analytical results of glulam's cross-sectional capacity

No.	Beam code	Moment M (N mm)	Load P (N)	Load x 1.4 P' (N)	Shear Force F _v (Mpa)	Actual Shear F _v (Mpa)
1	BLS00	7690334,94	10986,193	15380,6	4,4100	0,790
2	BLS25	5860441,337	8372,059	11720,8	4,4100	0,690
3	BLS50	4324162.500	6170,02	8638,2	4,4100	0,590
4	BLS75	2981441.406	4281,376	3852,6	4,4100	0,490
5	BLS100	1927341.000	2752,033	1926,3	4,4100	0,390



Picture 3: The comparison of glulam and analytical strength

The Stiffness of Glulam Beam

From the results of the glulam beam test, there were decreases of stiffness by 667.96 N/mm, 687.46N/mm, 586.85 N/mm, 568.18 N/mm, 448.12 N/mm. The average decrease in percentage for BLS 25% increased the stiffness by 102.9%. Glulam beams of 50%, 75%, and 100% were decreased sequentially by 87.86%, 85.06%, and 67.08%. It meant that 25% BLS beam could be used as structures beam due to rigidity increased by 2.9%, as shown in table 6.

Table 6. Stiffness Decrease of glulam beam

NO	Beam Code	Proportional load Limit	Deflection of Proportional Limit	Average Stiffness	Average Stiffness Decrease
		(N)	(mm)	(N/mm)	(%)
1	BLS 00	21000	31,92	667.96	100
2	BLS 25	16333,33	24,12	687.46	102.9
3	BLS 50	15500	26,42	586.85	87.86
4	BLS 75	14833,34	26,48	568,18	85,06
5	BLS100	5866,67	13,12	448,12	67,08

The decreases of moment and stiffness factors were obtained from various positions and the number of connections. Moment was decreased sequentially of 14116.67 KN/mm, 11316.67 KN/mm, 10966.67 KN/mm, 1033.34 KN/mm, and 3966.67 KN/mm. The stiffness factors were decreased sequentially of 1229.64 KN/M², 1054.87 KN/m², 745.23 KN/m², 516.66 KN/m², 275.06 KN/m² of which can be shown in table 7.

Table 7. Decrease of Moment and stiffness factor

No.	Beam Code	Average Moment	Average Curvature (x10 ⁶)	Average Stiffness Factor	Average decrease	Average Theoretical/ Test	Theoretical/ Test Average
		(KN-mm)	(1/mm)	(KN/m ²)	(%)		(%)
1	BLS 00	14116,67	11.310	1229,64	100	0,57	56
2	BLS 25	11316,67	10,280	1054,87	85.78	0,53	52
3	BLS 50	10966,67	13,52	745,23	60.61	0,42	42
4	BLS 75	1033,34	19,830	516,66	42.02	0,34	34
5	BLS100	3966,67	14,66	275,06	22.37	0.48	49

5. Conclusions and Suggestions

Conclusions

Based on the discussion of the research results conducted, it can be drawn some conclusions as follows:

- 1) The average moisture content of sengon wood was 12% accordance to Indonesia wood adhesive standards. The density was low in 0.271 t/m³ which included in strong class V according to PKKI-61. The Optimum adhesion constancy of phenol formaldehyde was 60/MDGL. The amount of adhesive spread was 322.23 gram/m². Modulus of elasticity (stiffness) was 5135,38MPa which meant that the forging of 1 to 1.1 MPa had not passed the elasticity of material.
- 2) The maximum strength of glulam timber was 32.00 MPa and stiffness of 25.00 Mpa. The various positions and number of connections were 0%, 25%, 50%, 75%, and 100%. They were decreased by 100%, 86.93%, 71.89%, 70.56%, and 29.28%. The stiffness was decreased by 100%, 99.92%, 87.86%, 83.06%, 67.08%. It meant that in position and number of connections of 25% and 50%, the decreases of strength and stiffness were relatively small so that it could be used as beam structure.
- 3) The damage of sengon glulam for all positions and the number of connections dominantly happened because of bending or the damage in the connection of the tensile area. However, loading less makes the percentage of connection sudden damage (shear) greater.

Suggestions

Some suggestions put forward for further research include:

- 1) Sengon should be included in strong class IV so that it can add the contribution of structural materials.
- 2) Wooden structured beam on long spans of sengon can be contributed, with relative small percentage of connections and placed on the compressive area.
- 3) Because glulam beam deflection has large percentage and the sudden collapse of the dominant structure (shear) for dry wood has less than 12 percent, the security and caution are needed.
- 4) The further researches for glulam beam with various kinds of connection constructions and some types of wood with other types of adhesives are needed.

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